

1) For steady-state, no light:

a)
$$D_n \frac{\partial^2 \Delta n_p}{\partial x^2} = \frac{\Delta n_p}{\tau_n} \quad (1)$$

Plug solution into (1) & see if satisfied:

$$D_n \frac{\partial^2 \Delta n_p}{\partial x^2} = \frac{D_n}{(L_n)^2} \Delta n_p(x) = \frac{\Delta n_p(x)}{\tau_n}$$

$$L_n = \sqrt{D_n \tau_n}$$

At $x=0$, $\Delta n(x) = \Delta n_B(0)$

At $x=W$, $\Delta n(x) = \Delta n_B(W)$

The distribution satisfies the minority carrier diffusion equation & the 2 boundary conditions. \Rightarrow it is the unique solution.

b)
$$I_{EN} = -q \frac{D_{nB}}{L_{nB}} \Delta n_B(0) \frac{\cosh\left(\frac{W-x}{L_{nB}}\right)}{\sinh\left(\frac{W}{L_{nB}}\right)} + \Delta n_B(W) q \frac{D_{nB}}{L_{nB}} \frac{\cosh\left(\frac{x}{L_{nB}}\right)}{\sinh\left(\frac{W}{L_{nB}}\right)}$$

$$I_{EN} = -q \frac{D_{nB}}{L_{nB}} \Delta n_B(0) \frac{\cosh\left(\frac{W}{L_{nB}}\right)}{\sinh\left(\frac{W}{L_{nB}}\right)} + \frac{q D_{nB} \Delta n_B(W)}{L_{nB}} \frac{1}{\sinh\left(\frac{W}{L_{nB}}\right)}$$

$$\Delta n_B(0) = \frac{n_i^2}{N_{AB}} (e^{V_{BE}/V_T} - 1) \quad \text{where } V_T = k_B T / q$$

$$\Delta n_B(W) = \frac{n_i^2}{N_{AB}} (e^{V_{BC}/V_T} - 1)$$

$$I_{cN} = +q \frac{D_{nB}}{L_{nB}} \frac{n_i^2}{N_{AB}} \left[\frac{-(e^{V_{BE}/V_T} - 1)}{\sinh\left(\frac{W}{L_{nB}}\right)} + \frac{(e^{V_{BC}/V_T} - 1) \cosh\left(\frac{W}{L_{nB}}\right)}{\sinh\left(\frac{W}{L_{nB}}\right)} \right]$$

c) Forward active region \Rightarrow only keep terms $\propto e^{V_{BE}/V_T}$

$$\alpha_T = \frac{I_{Cn}}{I_{En}} = \frac{1}{\cosh\left(\frac{W}{L_{nB}}\right)} \approx \frac{1}{1 + \frac{1}{2}\left(\frac{W}{L_{nB}}\right)^2}$$

$$\frac{W}{L_{nB}} \ll 1$$

d) From class notes:

$$I_{EP} = -q \frac{D_{PE}}{L_{PE}} \frac{n_i^2}{N_{DE}} e^{qV_{BE}/kT}$$

$$\frac{I_{EN}}{I_{EN} + I_{EP}} = \frac{\frac{D_{nB}}{L_{nB}} \frac{n_i^2}{N_{AB}} \frac{\cosh\left(\frac{W}{L_{nB}}\right)}{\sinh\left(\frac{W}{L_{nB}}\right)}}{I_{EN} + \frac{D_{PE}}{L_{PE}} \frac{n_i^2}{N_{DE}}}$$

$$\gamma = \frac{1}{1 + \frac{D_{PE}}{L_{PE}} \frac{L_{nB}}{D_{nB}} \frac{N_{AB}}{N_{DE}} \frac{\sinh\left(\frac{W}{L_{nB}}\right)}{\cosh\left(\frac{W}{L_{nB}}\right)}}$$

Keeping only terms to 1st order in $\frac{W}{L_{nB}}$:

$$\gamma \approx \frac{1}{1 + \frac{D_{PE}}{D_{nB}} \frac{L_{nB}}{L_{PE}} \frac{N_{AB}}{N_{DE}} \frac{W}{L_{nB}}}$$

$$2) I_C = -I_{RO} (e^{V_{BC}/V_T} - 1) + \alpha_F I_{FO} (e^{V_{BE}/V_T} - 1)$$

a)

$$V_{CE} = 0 \Rightarrow V_{EB} + V_{BC} = 0 \Rightarrow V_{BE} = V_{BC}$$

$$\text{so } I_C = (\alpha_F I_{FO} - I_{RO}) (e^{V_{BE}/V_T} - 1) \quad \text{where}$$

$$I_{FO} = q \left(\frac{D_{PE}}{L_{PE}} \frac{n_i^2}{N_{DE}} + \frac{D_{nB}}{L_{nB}} \frac{n_i^2}{N_{AB}} \right)$$

$$I_{RO} = q \left(\frac{D_{pC}}{L_{pC}} \frac{n_i^2}{N_{DC}} + \frac{D_{nB}}{L_{nB}} \frac{n_i^2}{N_{AB}} \right)$$

b) Assuming $\alpha_F \approx 1$,

$$\alpha_F I_{F0} - I_{R0} \approx q \left(\frac{D_{pE}}{L_{pE}} \frac{n_i^2}{N_{pE}} - \frac{D_{pC}}{L_{pC}} \frac{n_i^2}{N_{pC}} \right)$$

< 0 since $N_{pE} \sim 10^4 N_{pC}$

Also:

$$I_B = \frac{I_{F0}}{e^{V_{BE}/V_T} + 1}$$

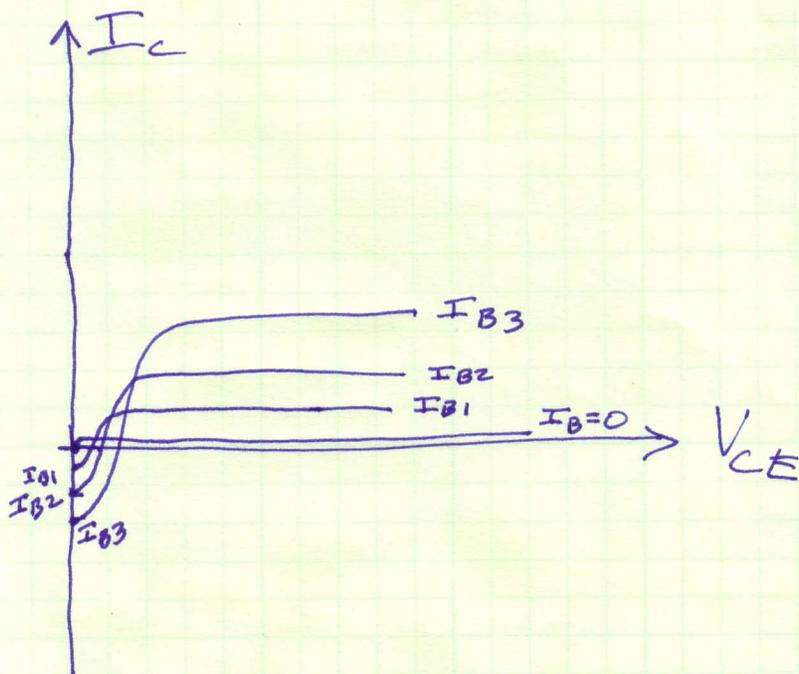
$$= \left[I_{F0} (1 - \alpha_F) + I_{R0} (1 - \alpha_R) \right] (e^{V_{BE}/V_T} - 1)$$

$$I_B = \left[\frac{I_{F0}}{\beta_F + 1} + \frac{I_{R0}}{\beta_R + 1} \right] (e^{V_{BE}/V_T} - 1)$$

At $V_{CE} = 0$, $I_B = 0 \Rightarrow V_{BE} = V_{BC} = 0$.

$$\Rightarrow I_C = 0$$

As $I_B \uparrow$, $V_{BE} \uparrow \Rightarrow I_C \downarrow$ at $V_{CE} = 0$.



3) with collector open:

$$\underbrace{I_{RO} \left(e^{V_{BC}/V_T} - 1 \right)}_{I_R} - \alpha_F I_F = 0$$
$$I_R = \alpha_F I_F$$

$$I_E = I_F - \alpha_R I_R = I_F (1 - \alpha_R \alpha_F)$$

$$I_E = I_{FO} (1 - \alpha_R \alpha_F) \left(e^{V_{BE}/V_T} - 1 \right) \quad (1)$$

With collector shorted to base:

$$V_{BC} = 0 \Rightarrow I_R = 0$$

$$I_E = I_{FO} \left(e^{V_{BE}/V_T} - 1 \right) \quad (2)$$

(2) > (1) \Rightarrow does make a difference.

w/ C open

$$I_{RO} \left(e^{V_{BC}/V_T} - 1 \right) = \alpha_F I_{FO} \left(e^{V_{BE}/V_T} - 1 \right)$$