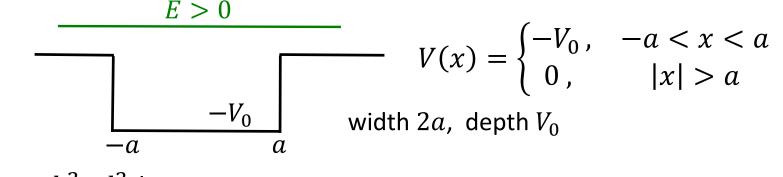
# EE201/MSE207 Lecture 6 Finite square well: scattering states



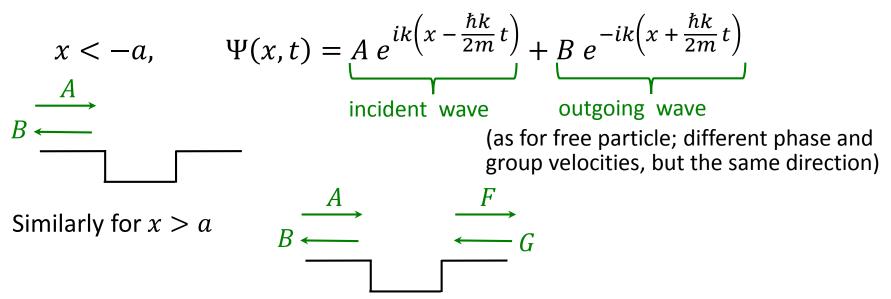
 $-\frac{\hbar^2}{2m}\frac{d^2\psi}{dx^2} + V(x)\psi = E\psi \qquad \text{Now }E \text{ is given (any energy is possible)}$ TISE

Again 3 regions:

x < -a,  $\psi(x) = A e^{ikx} + Be^{-ikx}$ ,  $k = \frac{\sqrt{2mE}}{\hbar}$  (definition of k as for free particle) |x| < a,  $\psi(x) = C \sin(lx) + D \cos(lx)$ ,  $l = \sqrt{2m(E + V_0)}/\hbar$  (as before) x > a,  $\psi(x) = F e^{ikx} + G e^{-ikx}$ 

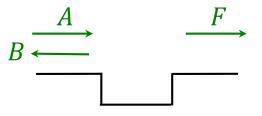
4 boundary conditions, 6 variables (E is given, no normalization) No hope to find unique solution. But there should not be a unique solution! Let us focus on physical meaning (important to find a proper question).

#### Add time dependence



(if necessary, wave packets can be constructed later; in reality nobody usually does it because it is too complicated; instead, people work with unnormalized states)

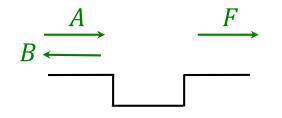
Assume that the wave is incident from the left, then G = 0



 $\begin{array}{ccc} F \\ & A \text{ is incident wave amplitude} \\ & B \text{ is reflected wave amplitude} \\ & F \text{ is transmitted wave amplitude} \\ \end{array}$ 

We have 5 variables (A, B, C, D, F) and 4 equations. Equations are linear. Can express B, C, D, F as functions of A (incident amplitude).

# **Proper questions**



A is incident wave amplitude *B* is reflected wave amplitude F is transmitted wave amplitude

(assume a wave incident from the left)

Goal: find ratios 
$$r = \frac{B}{A}$$
 and  $t = \frac{F}{A}$ 

(these ratios are called reflection and transmission amplitudes)

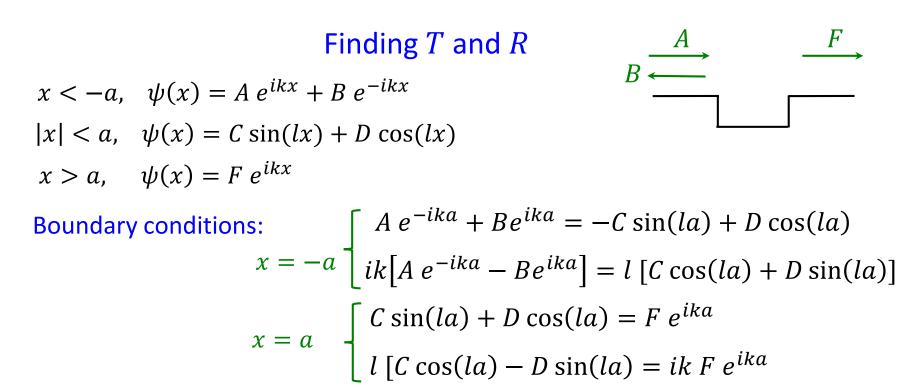
Reflection coefficient (probability of reflection)  $R = |r|^2 = \frac{|B|^2}{|A|^2}$ Transmission coefficient (probability of transmission)  $T = |t|^2 = \frac{|F|^2}{|A|^2}$ 

From physical meaning T + R = 1

Remark 1. Definition of T is sometimes different (discuss later,  $\times v_r/v_l$ )

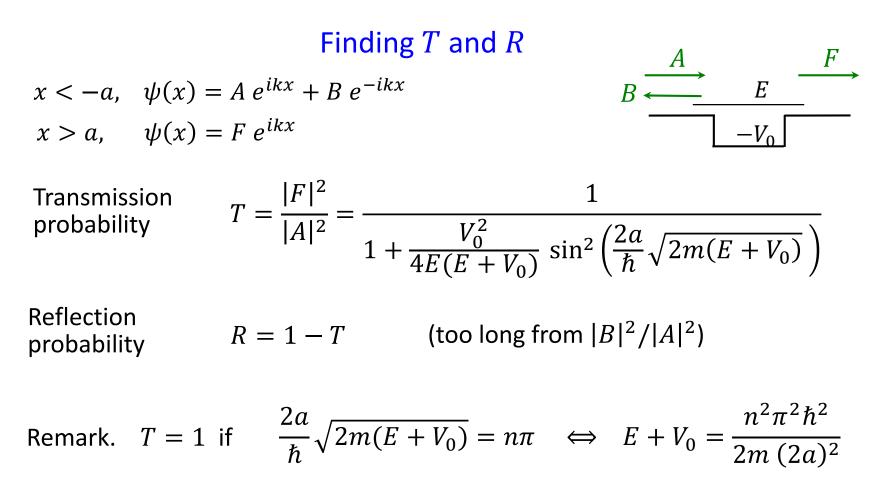
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Remark 2. Terminology: Reflection/transmission amplitudes (r, t)
                         and coefficients (R, T)
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Remark 3. We defined R and T as ratios; they become probabilities for wave packets (possible to show). Quadratic because probability  $\propto |\Psi|^2$ .



Simple to exclude C and D (similar combinations), then 2 equations with A, B, F

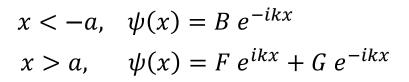
Finally
$$\begin{cases}
F = \frac{e^{-2ika}}{\cos(2la) - i\frac{\sin(2la)}{2kl}(k^2 + l^2)} A & k = \frac{\sqrt{2mE}}{\hbar} \\
B = i\frac{\sin(2la)}{2kl}(l^2 - k^2) F & l = \frac{\sqrt{2m(E + V_0)}}{\hbar}
\end{cases}$$

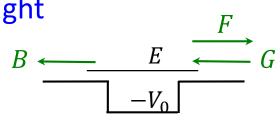


This is exactly the "simple" energy quantization (in infinite well).

Explanation: destructive interference of reflected waves (similar to anti-reflective coating with quarter-wavelength films).

# Now wave incident from the right





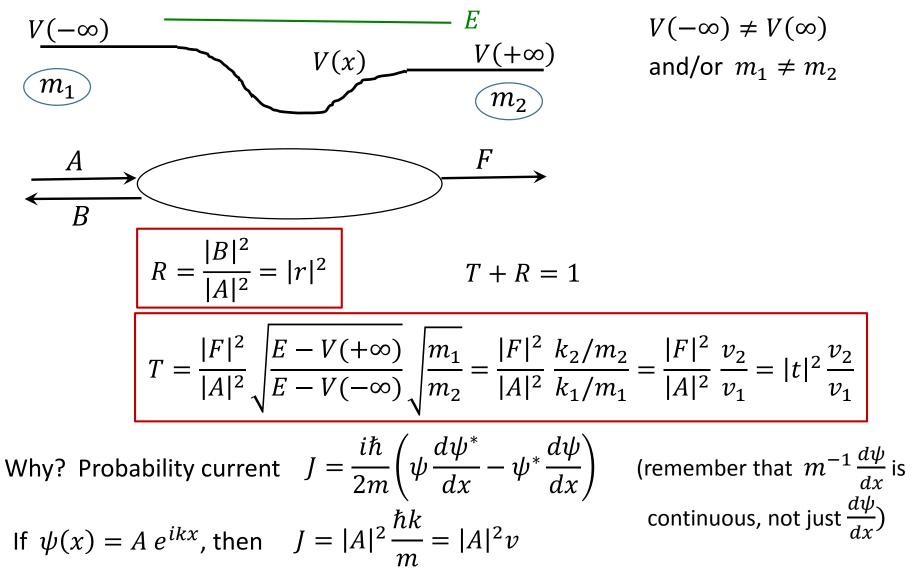
Similarly, we can find transmission and reflection coefficients

$$T_{\rm r} = |t_{\rm r}|^2 = \frac{|B|^2}{|G|^2}$$
  $R_{\rm r} = |r_{\rm r}|^2 = \frac{|F|^2}{|G|^2}$   $T_{\rm r} + R_{\rm r} = 1$ 

In our case because of symmetry  $T_r = T_l = T$  $R_r = T_l = R$ 

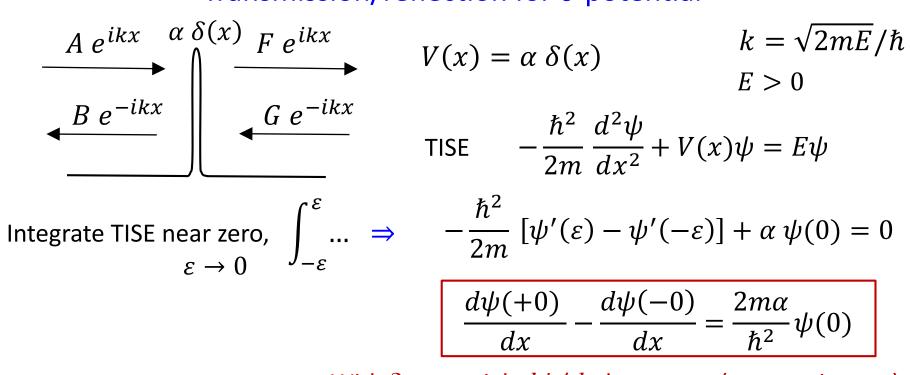
> However, this is always true (for any potential V(x)and possibly different masses)

# T and R in general case



The same velocity for reflection, but may be different for transmission

### Transmission/reflection for $\delta$ -potential



With  $\delta$ -potential,  $d\psi/dx$  has a step (not continuous).

 $\frac{1}{A} = \frac{1}{1+i\frac{m\alpha}{1+i}}$ 

Boundary conditions

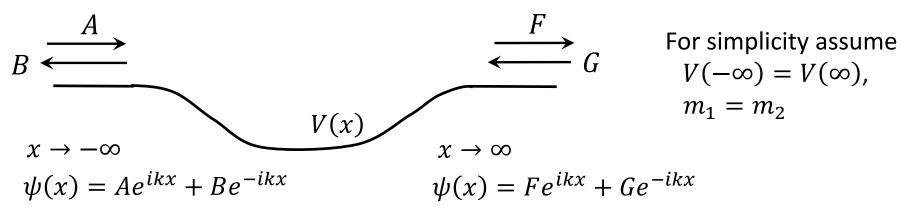
$$\begin{cases} A+B = F+G\\ ik(F-G) - ik(A-B) = \frac{2m\alpha}{\hbar^2}(A+B) \end{cases}$$

 $\frac{D}{A} = \frac{n^2 \kappa}{1 + i \frac{m\alpha}{k^2 L}},$ 

If G = 0 (incident from the left), then

#### [not included into this course]

Scattering matrix (now waves incident from both sides)



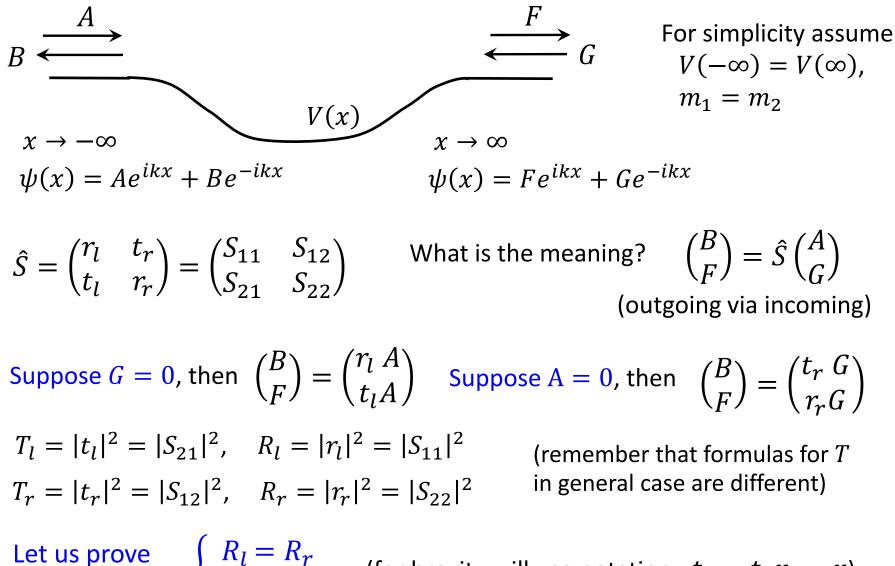
Out of 4 wave amplitudes (A, B, F, G), 2 free parameters, and the other 2 can be calculated (linear relations)

Why 2 free parameters? 1) it was 2 in rectangular well 2) TISE is a second-order dif. eq.  $\Rightarrow$  2 boundary conditions

Suppose we found transmission/reflection amplitudes  $(t_l, r_l)$  for the wave incident from the left and also from the right  $(t_r, r_r)$ . It is convenient to write these 4 complex numbers as a  $2 \times 2$  matrix.

$$\hat{S} = \begin{pmatrix} r_l & t_r \\ t_l & r_r \end{pmatrix} = \begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix}$$
 What is the meaning?  $\begin{pmatrix} B \\ F \end{pmatrix} = \hat{S} \begin{pmatrix} A \\ G \end{pmatrix}$  (scattering matrix) (outgoing via incoming)

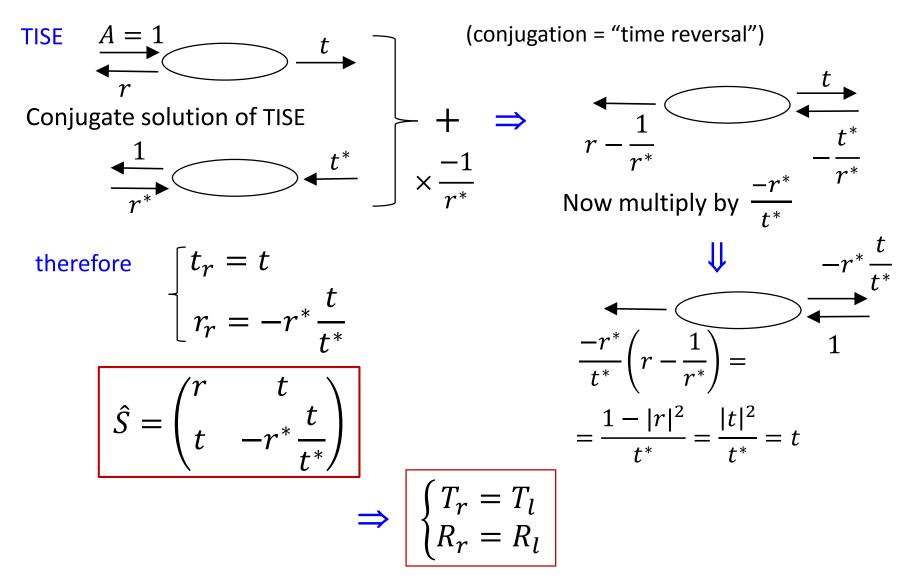
#### Scattering matrix (S-matrix)



Let us prove symmetry:  $\begin{cases} R_l = R_r \\ T_l = T_r \end{cases}$  (for brevity will use notation:  $t_l = t, r_l = r$ )

## Symmetry of the scattering matrix

Our proof will use "graphical operations" with solutions of TISE



# Symmetry of the S-matrix in general case

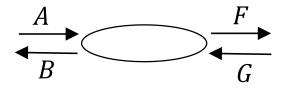
$$V(-\infty) \neq V(\infty), \ m_1 \neq m_2 \qquad \text{Without derivation, just a result}$$
Still  $r_r = -r^* \frac{t}{t^*} \qquad (\text{velocity } v_1 \text{ at the left, } v_2 \text{ at the right})$ 
But  $t_r = \frac{1 - |r|^2}{t^*} = \frac{|t|^2 \frac{v_2}{v_1}}{t^*} = t \frac{v_2}{v_1} \qquad \frac{v_2}{v_1} = \frac{k_2/m_2}{k_1/m_1}$ 

$$\widehat{S} = \begin{pmatrix} r & t \frac{v_2}{v_1} \\ t & -r^* \frac{t}{t^*} \end{pmatrix}$$
Then  $T_r = |t_r|^2 \frac{v_1}{v_2} = |t|^2 \frac{v_2}{v_1} = T_l$ 
 $R_r = R_l \qquad \Rightarrow \text{ still} \qquad \begin{cases} T_r = T_l \\ R_r = R_l \end{cases}$ 

#### [also not included into this course]

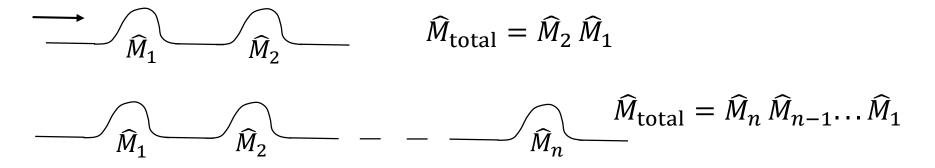
# Transfer matrix (M-matrix or T-matrix)

Sometimes instead of 
$$\begin{pmatrix} B \\ F \end{pmatrix} = \hat{S} \begin{pmatrix} A \\ G \end{pmatrix}$$
  
it is more convenient to use  $\begin{pmatrix} F \\ G \end{pmatrix} = \hat{M} \begin{pmatrix} A \\ B \end{pmatrix}$   
right left



(sometimes notation  $\widehat{T}$  instead of  $\widehat{M}$ )

If we know  $\hat{S}$ , then it is easy to calculate  $\hat{M}$ , and vice versa. Why  $\hat{M}$  is convenient?



For a multi-barrier structure, all  $\widehat{M}_i$  are similar, therefore it is simple to calculate  $\widehat{M}_{total}$ . (Actually, each  $\widehat{M}_i$  also contains a phase factor, depending on *x*-position.)

## M-matrix: symmetries and relation to S-matrix

(simple case,  $v_1 = v_2$ )

Symmetries of M-matrix
 1) 
$$M_{22} = M_{11}^*$$

 2)  $M_{12} = M_{21}^*$ 

 3) det  $\widehat{M} = 1$ 

(can be derived from symmetries of S-matrix)

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$$\begin{pmatrix} B \\ F \end{pmatrix} = \begin{pmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{pmatrix} \begin{pmatrix} A \\ G \end{pmatrix} \qquad \begin{pmatrix} F \\ G \end{pmatrix} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \begin{pmatrix} A \\ B \end{pmatrix}$$

Conversion

$$S_{11} = -\frac{M_{21}}{M_{22}} = -\frac{M_{12}^*}{M_{22}} \qquad M_{11} = \frac{1}{S_{12}^*} = \frac{1}{S_{21}^*}$$
$$S_{22} = \frac{M_{12}}{M_{22}} \qquad M_{22} = \frac{1}{S_{12}}$$
$$M_{22} = \frac{1}{S_{12}}$$
$$M_{12} = -\frac{S_{11}^*}{S_{12}^*} = \frac{S_{22}}{S_{12}}$$
$$M_{21} = -\frac{S_{11}}{S_{12}}$$